

Category		Title
NFR:	1.B.1.b	Fugitive emissions from solid fuels: Solid fuel transformation
SNAP:	040201 040204	Coke oven (door leakage and extinction) Solid smokeless fuel
ISIC:		
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1 Overview

This source category discusses emissions from coke ovens (only fugitive emissions from door leakages and extinction; emissions from the furnace are covered by the relevant combustion chapter) and emissions from the production of solid smokeless fuel (during coal carbonisation).

Coke production in general can be divided into coal handling and storage, coke oven charging, coal coking, extinction of coke and coke oven-gas purification. Combustion in coke oven furnaces is treated in chapter 1.A.1.c; the fugitive emissions from door leakage and extinction are covered by this chapter. Door leakage and extinction lead to emissions of all major pollutants including heavy metals and POPs.

Solid smokeless fuel has been used for a long time by householders in open fire grates in the past (Parker, 1978). Fugitive emissions during coal carbonisation for the production of solid smokeless fuel are considered to be small. Very limited information is available. It is expected that the emissions include sulphur and nitrogen oxides, VOCs (NMVOC (non-methane volatile organic compounds) as well as methane), volatile heavy metals and POPs from coal. A coal carbonisation plant can be an important source of air contamination on a local scale.

2 Description of sources

This section describes the coke production process as well as the production process of solid smokeless fuel.

2.1 Process description

2.1.1 *Coke oven*

About 90 % of the coke consumed in the EU is used in pig iron production. The major part is used in blast furnaces, followed by iron foundries, non-ferrous smelters, and the chemical industry.

Figure 2-1 gives a simple process scheme, displaying the emissions from coke production.

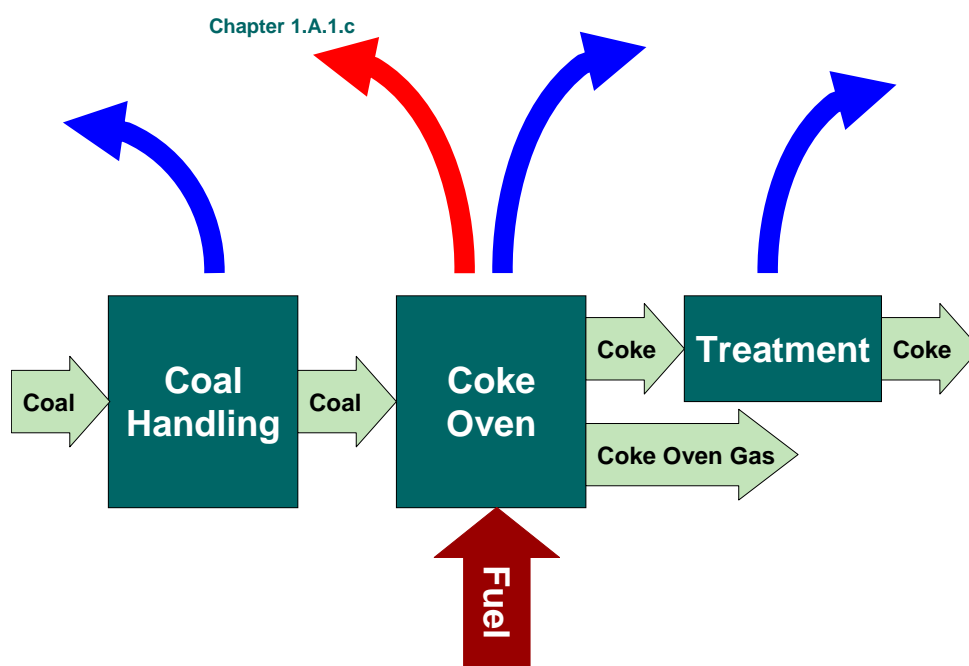


Figure 2-1 Process scheme for coke production, the most important process within source category 1.B.1.b Solid fuel transformation; combustion emissions from the coke oven are treated in chapter 1.A.1.c

Coke and coke by-products (including coke oven gas) are produced by the pyrolysis (heating in the absence of air) of suitable grades of coal. The process also includes the processing of coke oven gas to remove tar, ammonia (usually recovered as ammonium sulphate), phenol, naphthalene, light oil, and sulphur before being used as a fuel for heating the ovens (World Bank Group, 1997).

For coke production, hard coal is crushed, mixed and sieved. The coal is transported to the coke oven, which is charged by the mixture. After heating for 14 to 36 hours at 1 150 –1 350 °C in the absence of oxygen, the coked mixture is pressed out of the coke chambers into special wagons. Subsequently, the hot coke will be extinguished.

The emissions related to coke production can be attributed to four sub-processes, namely:

- coal handling and storage: emitting coal dust;
- coke production and extinction: emitting coal and coke dust and coke oven gas;
- coke oven gas handling and purification: emitting benzene, toluene, xylene, phenol, PAH (polycyclic aromatic hydrocarbons), H₂S, HCN and NH₃;
- combustion of coke oven gas: emitting C_xH_y, SO₂, NO_x, CO, CO₂, HF and soot.

Coke oven gas may be burned to heat the coke oven, or transferred off site (e.g. into the natural gas distribution system) and used as an energy source.

2.1.2 Solid smokeless fuel

Coal carbonisation to produce solid smokeless fuel occurs at high temperatures reaching 1 000 °C. There are three methods of coal carbonisation which differ considerably from each other. In the first method, the coal is carbonised in tubular iron retorts heated externally by the gas produced. In the second, the coal is in a large chamber and is heated by direct contact with the products of combustion of the gas made. In both cases the product reactive coke is screened to obtain sizes suitable for the open fire and for closed stoves. In the third method, the coal is carbonised by fluidization with hot gas from combustion of the coal gas made, and the relatively small particles are pressed to form briquettes (Parker, 1978). A general process scheme is given below.

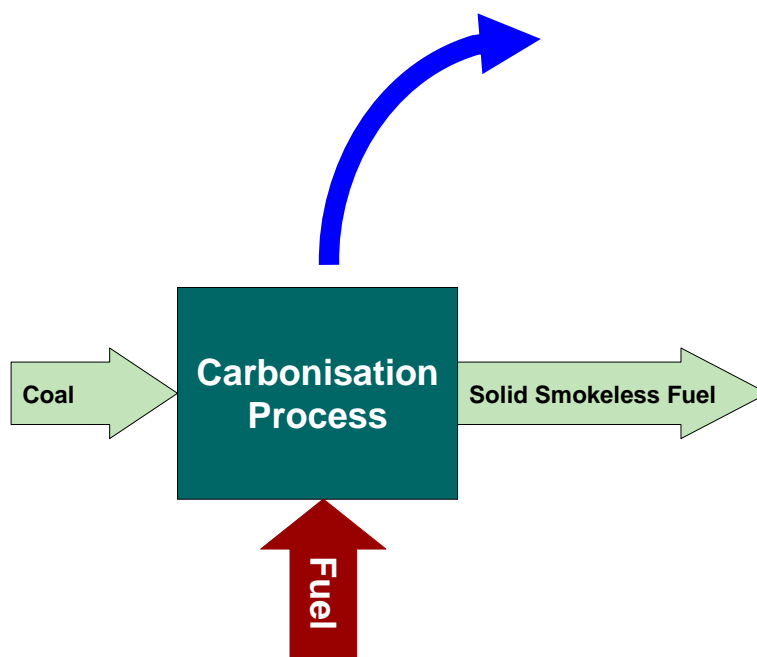


Figure 2-2 Process scheme for the production of solid smokeless fuel from coal

There are also systems for making solid smokeless fuel in which only certain types of coal, for example anthracite duff, are briquetted with pitch at a suitable temperature and then carbonised.

Modern coal carbonisation plants are equipped with electrostatic precipitators that remove at least 98 % of the particulate matter from exhaust gases.

2.2 Techniques

In the coke making process, bituminous coal is fed (usually after processing operations, which control the size and the quality of the feed) into a series of ovens. The coke oven itself is a chamber, built of heat resistant bricks, generally 0.4–0.7 m wide, 4–8 m high and 12–18 m long. A chamber has two doors, one at each end, covering almost the full cross-sectional area. In the roof, there are 3–5 charging holes and a gas outlet ('ascension pipe'). Commonly 40 to 70 chambers, alternating with heating walls, form a coke oven battery (Dutch notes on Best Available Techniques (BAT) 1997). Combustion of gases in burners in the flues between the ovens provides heat for the process. In order to improve the energy efficiency, regenerators are located right under

the ovens, exchanging heat from flue gases with combustion air or fuel. Coke oven gas from the by-product recovery plant is the common fuel for under-firing the ovens at most plants, but blast furnace gas, and infrequently, natural gas may also be used (US Environmental Protection Agency (US EPA), 1985a).

The ovens are sealed and heated at high temperatures. The generation of steam, gases, and organic compounds starts immediately after charging and they are exhausted via ascension pipes into the crude gas collecting system (Dutch notes on BAT 1997). Volatile compounds are processed to recover combustible gases and other by-products. After coking, the vertical doors on each end of an oven are removed; a long ram pushes the coke from the oven into a rail quench car, which goes to a quench tower. There, large volumes of water are sprayed onto the coke mass to cool it, so that it will not continue to burn after being exposed to air. Alternatively, circulating an inert gas (nitrogen), also known as dry quenching, can cool it. Coke is screened and sent to a blast furnace or for storage.

The raw coke oven gas exits at temperatures of about 760 to 870 °C and is shock cooled by spraying recycled flushing liquor in the gooseneck. This spray cools the gas to 80 to 100 °C, precipitates tar, condenses various vapours, and serves as the carrying medium for the condensed compounds. These products are separated from the liquor in a decanter and are subsequently processed to yield tar and tar derivatives (US EPA 1985b, van Osdell et al. 1979).

The gas is then passed either to a final tar extractor or an electrostatic precipitator for additional tar removal. When the gas leaves the tar extractor, it carries 75 % of the ammonia and 95 % of the light oil originally present when leaving the oven. The ammonia is recovered either as an aqueous solution by water absorption or as ammonium sulphate salt. The gas leaving the saturator at about 60 °C is taken to final coolers or condensers, where it is typically cooled with water to approximately 24 °C. During this cooling, some naphthalene separates and is carried along with the wastewater and recovered. The remaining gas is passed into a light oil or benzene scrubber, over which is circulated a heavy petroleum fraction called wash oil or a coal-tar oil, which serves as the absorbent medium. The oil is sprayed in the top of the packed absorption tower while the gas flows up through the tower. The wash oil absorbs about 2 to 3 % of its weight of light oil, with a removal efficiency of about 95 % of the light oil vapour in the gas. The rich wash oil is passed to a counter current steam stripping column. The steam and light oil vapours pass upward from the still, through a heat exchanger to a condenser and water separator. The light oil may be sold as crude or processed to recover benzene, toluene, xylene, and solvent naphtha (US EPA 1985b, van Osdell et al. 1979).

After tar, ammonia, and light oil removal, the gas undergoes final desulphurisation (e. g. by the Claus process) at some coke plants before being used as fuel. The coke oven gas has a rather high heating value, in the order of 20 kJ/m³ (STP). Typically, 35 to 40 % of the gas is returned to fuel the coke oven combustion system, and the remainder is used for other plant heating needs (US EPA 1985b, van Osdell et al. 1979).

Although most benzene is obtained from petroleum, some is recovered through distillation of coke oven light oil at coke by-product plants. Light oil is clear yellow-brown oil which contains coal gas components with boiling points between 0 and 200 °C (van Osdell et al. 1979). Most by-product plants recover light oil, but not all plants refine it. About 13–18 l of light oil can be produced from coke ovens producing 1 mg of furnace coke. Light oil itself contains from 60 to 85 % benzene (US EPA, 1985a; Loibl et al., 1993).

2.3 Emissions

The coke oven is a major source of fugitive emissions into the air. The coking process emits sulphur oxides (SO_x), nitrogen oxides (NO_x), volatile organic compounds (non-methane VOC and methane (CH₄)), carbon dioxide (CO₂), carbon monoxide (CO), ammonia (NH₃), particulate matter, and heavy metals. In general, emissions of nitrous oxide (N₂O) are not relevant. Coke ovens are an important source of PAH emissions (polycyclic aromatic hydrocarbons).

The components of coke oven gas (raw gas) and their concentrations are given in Table 2-1.

Table 2-1 Composition of raw coke oven gas (adapted from Winnacker, 1982)

Components of coke oven gas	Concentration [Vol.-%]
H ₂	58–65
CH ₄	24–29
CO	4.6–6.8
C _x H _y	2–4
CO ₂	1.5–2.5

Besides these compounds, the following by-products are also components of the coke oven gas produced: tar, phenol, benzene, pyridine, ammonia, H₂S, HCN and CS₂ (carbon bisulphide) (Winnacker 1982). The by-product recovery section of a coking plant (e.g. ammonia processing, tar processing) may release significant amounts of NMVOC, CH₄, NH₃ and particulate matter (covered by SNAP code 040201).

Furthermore, continuous and discontinuous releases of emissions into the air can be distinguished (Dutch notes on BAT 1997):

Continuous emissions to air:

- emissions from storage and handling of raw materials and products,
- oven door and frame seal leakage,
- ascension pipe leakage,
- charging holes leakage,
- coke oven firing,
- vent systems in gas treatment plant,
- desulphurisation plant.

Discontinuous emissions to air:

- oven charging,
- coke pushing,
- coke cooling.

2.4 Controls

Charging:

Dust particles from coal charging can be evacuated by the use of jumper-pipe system and steam injection into the ascension pipe or controlled by fabric filters (World Bank Group 1997).

Coking:

Emissions decrease with the increase of the size of the ovens. Large ovens increase batch size and reduce the necessary charging and pushing, thereby reducing associated emissions. Emissions are also reduced by constant coking conditions, cleaning, and a low-leakage door construction e. g. with gas sealing (Dutch notes on BAT 1997).

Pushing:

Emissions from coke pushing can be reduced by maintaining a sufficient coking time thus avoiding the so-called 'green push'. Fugitive emissions can be controlled by sheds, enclosed cars or travelling hoods. It is good practice to treat captured gases in fabric filters (World Bank Group 1997).

Quenching:

Dry quenching creates lower emissions compared to wet quenching. Gases released from the dry quenching unit can be extracted and filtered. In the case of wet quenching, measures have to be taken to prevent pollutant transfer from wastewater to the air (Dutch notes on BAT 1997).

By-product recovery:

In the processing of light oil, tar, naphthalene, phenol, and ammonia, vapour recovery systems can be used. Tail gases from desulphurisation (Claus plant) can be returned to the coke oven gas system.

Combustion of coke oven gas:

Flue gases from coke oven firing contain NO_x, SO₂ and particulate matter as main pollutants. SO₂ emissions depend on the degree of desulphurisation of the coke oven gas. NO_x emissions may be reduced by low-NO_x-firing techniques.

3 Methods

3.1 Choice of method

Figure 3-1 presents the procedure to select the methods for estimating emissions from solid fuel transformation. The basic idea is:

- if detailed information is available, use it;
- if the source category is a key category, a Tier 2 or better method must be applied and detailed input data must be collected. The decision tree directs the user in such cases to the Tier 2 method, since it is expected that it is more easy to obtain the necessary input data for this approach than to collect facility level data needed for a Tier 3 estimate;
- the alternative of applying a Tier 3 method, using detailed process modelling, is not explicitly included in this decision tree. However, detailed modelling will always be done at facility level and results of such modelling could be seen as 'facility data' in the decision tree.

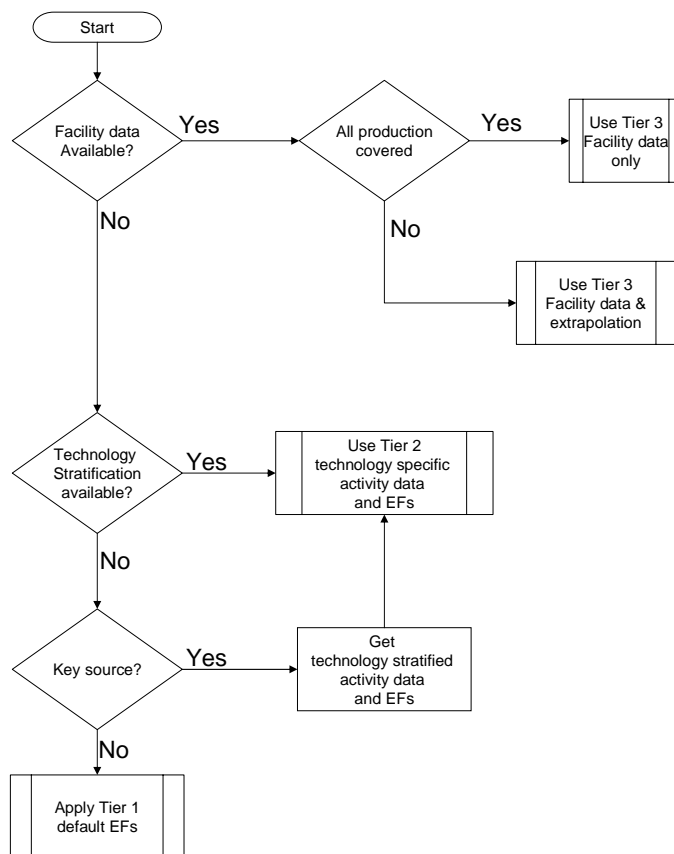


Figure 3-1 Decision tree for source category 1.B.1.b Solid fuel transformation

3.2 Tier 1 default approach

3.2.1 Algorithm

The Tier 1 approach for solid fuel transformation uses the general equation:

$$E_{\text{pollutant}} = AR_{\text{production}} \times EF_{\text{pollutant}} \quad (1)$$

where:

- $E_{\text{pollutant}}$ = the emission of the specified pollutant,
- $AR_{\text{production}}$ = the activity rate for the solid fuel transformation,
- $EF_{\text{pollutant}}$ = the emission factor for this pollutant.

This equation is applied at the national level, using the total solid fuel transformation (usually expressed in mass of coal carbonised or mass of coke produced).

The Tier 1 emission factors assume an averaged or typical technology and abatement implementation in the country and integrate all different sub-processes within the solid fuel transformation process.

In cases where specific abatement options are to be taken into account, a Tier 1 method is not applicable and a Tier 2 or Tier 3 approach must be used.

3.2.2 Default emission factors

This section presents the Tier 1 emission factors for solid fuel transformation. The production of coke is considered to be the most important process in this source category and is therefore used as the Tier 1 approach. In the Tier 2 approach, the production of solid smokeless fuel is also considered.

Default emission factors for coke production are taken from the BREF document for Iron and steel production (European Commission, 2001), which also includes the production of coke. These emission factors are originally given in mass per tonne liquid steel produced, and recalculated in terms of mass of coke produced using the suggested conversion factor of 0.34 tonne coke per tonne liquid steel (358 kg coke/tonne pig iron and 940 kg pig iron/tonne liquid steel).

No emission factors of NO_x, SO_x and CO are provided, since it is believed that these pollutants mainly originate from the combustion in the coke production process. Guidance on estimating these emissions is given in source category 1.A.1.c.

Emission factors in the BREF documents are mostly given in ranges. The range is interpreted as the 95 % confidence interval, while the geometric mean of this range is chosen as the value for the emission factor in the table below.

Table 3-1 Tier 1 emission factors for source category 1.B.1.b Solid fuel transformation

Tier 1 default emission factors					
	Code	Name			
NFR Source Category	1.B.1.b	Solid fuel transformation			
Fuel	NA				
Not applicable	Aldrin, Chlordane, Chlordecone, Dieldrin, Endrin, Heptachlor, Heptabromo-biphenyl, Mirex, Toxaphene, HCH, DDT, PCB, PCDD/F, HCB, PCP, SCCP				
Not estimated	NO _x , CO, SO _x , Cr, Cu, Se, Zn				
Pollutant	Value	Unit	95% confidence interval		Reference
			Lower	Upper	
NMVOG	17	g/Mg coke produced	12	24	European Commission (2001)
NH ₃	5	g/Mg coke produced	2	10	European Commission (2001)
TSP	110	g/Mg coke produced	50	200	European Commission (2001)
PM ₁₀	100	g/Mg coke produced	45	180	Estimation fraction of TSP based on US EPA data
PM _{2.5}	90	g/Mg coke produced	40	160	Estimation fraction of TSP based on US EPA data
Pb	1.2	g/Mg coke produced	0.6	1.7	Theloke et al. (2008)
Cd	0.03	g/Mg coke produced	0.02	0.04	Theloke et al. (2008)
Hg	0.02	g/Mg coke produced	0.01	0.03	Theloke et al. (2008)
As	0.1	g/Mg coke produced	0.08	0.2	Theloke et al. (2008)
Ni	0.3	g/Mg coke produced	0.2	0.3	Theloke et al. (2008)
Benzo(a)pyrene	0.75	g/Mg coke produced	0.3	2	Berdowski et al. (1995)
Benzo(b)fluoranthene	0.25	g/Mg coke produced	0.1	1	Berdowski et al. (1995)
Benzo(k)fluoranthene	0.25	g/Mg coke produced	0.1	1	Berdowski et al. (1995)
Indeno(1,2,3-cd)pyrene	0.3	g/Mg coke produced	0.1	1	Berdowski et al. (1995)
Total 4 PAHs	0.9	g/Mg coke produced	0.5	1.5	European Commission (2001)

3.2.3 Activity data

For activity data for the production of coke, the standard statistics on coke production and fuel consumption (e.g. International Energy Agency, United Nations, Eurostat, International Iron and Steel Institute, etc.).

3.3 Tier 2 technology-specific approach

3.3.1 Algorithm

The Tier 2 approach is similar to the Tier 1 approach. To apply the Tier 2 approach, both the activity data and the emission factors need to be stratified according to the different techniques that may occur in the country.

The approach followed to apply a Tier 2 approach is as follows.

Stratify the solid fuel transformation in the country to model the different product and process types occurring in the national industry into the inventory by:

- defining the production using each of the separate product and/or process types (together called ‘technologies’ in the formulae below) separately; and
- applying technology-specific emission factors for each process type:

$$E_{\text{pollutant}} = \sum_{\text{technologies}} AR_{\text{production,technology}} \times EF_{\text{technology,pollutant}} \quad (2)$$

where:

$AR_{\text{production,technology}}$ = the production rate within the source category, for the specific technology,

$EF_{\text{technology,pollutant}}$ = the emission factor for this technology and this pollutant.

A country where only one technology is implemented will result in a penetration factor of 100 % and the algorithm reduces to:

$$E_{\text{pollutant}} = AR_{\text{production}} \times EF_{\text{technology,pollutant}} \quad (3)$$

where:

$E_{\text{pollutant}}$ = the emission of the specified pollutant,

$AR_{\text{production}}$ = the activity rate for solid fuel transformation,

$EF_{\text{pollutant}}$ = the emission factor for this pollutant.

The emission factors in this approach will still include all sub-processes within the solid fuel transformation.

3.3.2 Technology-specific emission factors

This section presents the Tier 2 emission factors for emissions from solid fuel transformation. Two separate processes are distinguished; these are the production of coke in coke ovens and the production of solid smokeless fuel.

Emission estimates are provided in the tables below. As in the Tier 1 approach, emissions from NO_x , SO_x and CO for the coke oven are not given in this chapter, since they are assumed to originate mainly from combustion. Further guidance for these pollutants is provided in source category 1.A.1.c.

For solid smokeless fuel production, very little information on emission factors is available. Parker (1978) indicates that the waste gases from heating a range of retorts carbonising

1 000 tonnes of coal per day would contain a quantity of sulphur dioxide of about 2.5 tonnes per day.

Emission factors in the BREF documents are mostly given in ranges. The range is interpreted as the 95 % confidence interval, while the geometric mean of this range is chosen as the value for the emission factor in the table below.

Table 3-2 Tier 2 emission factors for source category 1.B.1.b Solid fuel transformation, Coke oven

Tier 2 emission factors					
	Code	Name			
NFR Source Category	1.B.1.b	Solid fuel transformation			
Fuel	NA				
SNAP (if applicable)	040201	Coke oven (door leakage and extinction)			
Technologies/Practices	Coke oven plant				
Region or regional conditions					
Abatement technologies					
Not applicable	Aldrin, Chlordane, Chlordecone, Dieldrin, Endrin, Heptachlor, Heptabromo-biphenyl, Mirex, Toxaphene, HCH, DDT, PCB, PCDD/F, HCB, PCP, SCCP				
Not estimated	NO _x , CO, SO _x , Cr, Cu, Se, Zn				
Pollutant	Value	Unit	95% confidence interval		Reference
			Lower	Upper	
NMVOC	17	g/Mg coke produced	12	24	European Commission (2001)
NH ₃	5	g/Mg coke produced	2	10	European Commission (2001)
TSP	110	g/Mg coke produced	50	200	European Commission (2001)
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PM _{2.5}	90	g/Mg coke produced	40	160	Estimation fraction of TSP based on US EPA data
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Cd	0.03	g/Mg coke produced	0.02	0.04	Theloke et al. (2008)
Hg	0.02	g/Mg coke produced	0.01	0.03	Theloke et al. (2008)
As	0.1	g/Mg coke produced	0.08	0.2	Theloke et al. (2008)
Ni	0.3	g/Mg coke produced	0.2	0.3	Theloke et al. (2008)
Benzo(a)pyrene	0.75	g/Mg coke produced	0.3	2	Berdowski et al. (1995)
Benzo(b)fluoranthene	0.25	g/Mg coke produced	0.1	1	Berdowski et al. (1995)
Benzo(k)fluoranthene	0.25	g/Mg coke produced	0.1	1	Berdowski et al. (1995)
Indeno(1,2,3-cd)pyrene	0.3	g/Mg coke produced	0.1	1	Berdowski et al. (1995)
Total 4 PAHs	0.9	g/Mg coke produced	0.5	1.5	European Commission (2001)

Table 3-3 Tier 2 emission factors for source category 1.B.1.b Solid Fuel Transformation, Solid smokeless fuel

Tier 2 emission factors					
	Code	Name			
NFR Source Category	1.B.1.b	Solid fuel transformation			
Fuel	NA				
SNAP (if applicable)	040204	Solid smokeless fuel			
Technologies/Practices	Solid smokeless fuel				
Region or regional conditions					
Abatement technologies					
Not applicable	Aldrin, Chlordane, Chlordecone, Dieldrin, Endrin, Heptachlor, Heptabromo-biphenyl, Mirex, Toxaphene, HCH, DDT, PCB, PCDD/F, HCB, PCP, SCCP				
Not estimated	NO _x , CO, NMVOC, NH ₃ , TSP, PM ₁₀ , PM _{2.5} , Pb, Cd, Hg, As, Cr, Cu, Ni, Se, Zn, Benzo(a)pyrene, Benzo(b)fluoranthene, Benzo(k)fluoranthene, Indeno(1,2,3-cd)pyrene, Total 4 PAHs				
Pollutant	Value	Unit	95% confidence interval		Reference
			Lower	Upper	
SO _x	2.5	kg/Mg coal carbonised	0	10	Parker (1978)

3.3.3 Abatement

No information available.

3.4 Tier 3 Emission modelling and use of facility data

This section provides Tier 3 information for coke production plants only. It is good practice to note again that only the fugitive emissions should be reported in this source category. It is good practice to report emissions from combustion within the coke production process in source category 1.A.1.c.

3.4.1 Algorithm

There are two different methods to apply emission estimation methods that go beyond the technology specific approach described above:

- detailed modelling of the process;
- using facility-level emission reports.

3.4.1.1 Detailed process modelling

A Tier 3 emission estimate, using process details will make separate estimates for the consecutive steps in the coke production process:

- coal handling,
- the coking process (without combustion),
- coke oven gas purification.

For emissions of particulate matter, an even more detailed process split is available.

3.4.1.2 Facility-level data

Where facility-level emission data of sufficient quality are available (see chapter 6, Inventory management, improvement and QA/QC in part A), it is good practice to indeed use these data. There are two possibilities:

- the facility reports cover all the coke production facilities in the country;
- facility-level emission reports are not available for all coke production plants in the country.

If facility-level data are covering all coke production in the country, it is good practice to compare the implied emission factors (reported emissions divided by the national lime production) with the default emission factor values or technology-specific emission factors. If the implied emission factors are outside the 95 % confidence intervals for the values given below, it is good practice to explain the reasons for this in the inventory report.

If the total annual coke production in the country is not included in the total of the facility reports, it is good practice to estimate the missing part of the national total emissions from the source using extrapolation by applying:

$$E_{Total, pollutant} = \sum_{Facilities} E_{Facility, pollutant} + \left(National\ Production - \sum_{Facilities} Production_{Facility} \right) \times EF \quad (4)$$

where

- $E_{total, pollutant}$ = the total emission of a pollutant for all facilities within the source category,
- $E_{facility, pollutant}$ = the emission of the pollutant as reported by a facility,

$Production_{total}$ = the production rate in the source category,

$Production_{facility}$ = the production rate in a facility,

$EF_{pollutant}$ = the emission factor for the pollutant.

Depending on the specific national circumstances and the coverage of the facility level reports as compared to the total national coke production, it is good practice to choose the emission factor (EF) in this equation from the following possibilities, in decreasing order of preference:

- technology-specific emission factors, based on knowledge of the types of technologies implemented at the facilities where facility-level emission reports are not available;
- the implied emission factor derived from the available emission reports:

$$EF = \frac{\sum_{Facilities} E_{Facility, pollutant}}{\sum_{Facilities} Production_{Facility}} \quad (5)$$

- the default Tier 1 emission factor. It is only good practice to choose this option if the facility-level emission reports cover more than 90 % of the total national production.

3.4.2 Tier 3: emission modelling and use of facility data

To apply a Tier 3 method for process modelling, the use of AP-42 is advised. For more information see US EPA (2007).

3.4.3 Activity data

The detailed Tier 3 methodology needs activity statistics for each of the different sub processes. Detailed information about the local situation is necessary.

4 Data quality

4.1 Completeness

No specific issues.

4.2 Avoiding double counting with other sectors

Care should be taken not to double count emissions from this process. Emissions from the combustion in the coke production should be reported in source category 1.A.1.c.

4.3 Verification

4.3.1 Best Available Technique emission factors

Information on Best Available Technique for coke production plants is available from the reference document for Best Available Technologies in the iron and steel industry.

Achievable emission levels associated with the use of BAT are available in this document for sub processes within the coke production.

4.4 Developing a consistent time series and recalculation

No specific issues.

4.5 Uncertainty assessment

4.5.1 *Emission factor uncertainties*

The uncertainty in the emission factors is estimated to be B–C. The General Guidance chapter on Uncertainties does provide information on how to quantify these quality ratings.

4.5.2 *Activity data uncertainties*

No specific issues.

4.6 Inventory quality assurance/quality control QA/QC

No specific issues.

4.7 Gridding

No specific issues.

4.8 Reporting and documentation

No specific issues.

5 Glossary

Coke oven gas	The gas formed during coking of coal
Extinction of coke	Cooling of the hot coke after removal from the coke chambers
Production of coke	Heating of coal mixtures in absence of oxygen at high temperatures

6 References

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7 Point of enquiry

Enquiries concerning this chapter should be directed to the relevant leader(s) of the Task Force on Emission Inventories and Projection's expert panel on combustion and industry. Please refer to the TFEIP website (www.tfeip-secretariat.org/) for the contact details of the current expert panel leaders.