WASTE INCINERATION Flaring in Oil Refinery

**SNAP CODE:** 

090203

109.03.11

1 B 2 c

**SOURCE ACTIVITY TITLE:** 

**NOSE CODE:** 

**NFR CODE:** 

#### **1** ACTIVITIES INCLUDED

Flares are commonly used during petroleum refining for the safe disposal of waste gases during process upsets (e.g., start-up, shut-down, system blow-down) and emergencies to combust the organic content of waste emission streams without recovering/using the associated energy.

#### 2 CONTRIBUTION TO TOTAL EMISSIONS

Although flaring emission estimates are approximate, total hydrocarbon emissions from flaring at Canadian petroleum refineries during 1988 represented about 0.1% of the refinery sector process and fugitive emissions that also included petroleum marketing emissions (CPPE, 1990). Thus the flaring operation at refineries is estimated to contribute a very small fraction of the total HC emissions in Canada. Emissions from flaring activities may also include: particulate, SOx, NOx, CO and other NMVOC. The CO<sub>2</sub> contribution of both miscellaneous vent and flare emission sources represented approximately 9% of the total petroleum refinery SO<sub>2</sub> emission in Canada during 1988.

Emissions estimates from flaring in petroleum refineries as reported in the CORINAIR90 inventory are summarised in Table 1.

Source-activity	SNAP-code	Contribution to total emissions [%]							
		$SO_2$	NO <sub>x</sub>	NMVOC	$CH_4$	CO	$CO_2$	$N_2O$	NH <sub>3</sub>
Flaring in Petroleum Refineries	090203	0.1	0.1	0	1	0	0	-	-

 Table 1: Contribution to total emissions of the CORINAIR90 inventory (28 countries)

0 = emissions are reported, but the exact value is below the rounding limit (0.1 per cent)

- = no emissions are reported

This activity is not believed to be a significant source of  $PM_{2.5}$  (as of December 2006).<sup>1</sup>

<sup>&</sup>lt;sup>1</sup> Updated with particulate matter details by: Mike Woodfield, AEA Technology, UK, December 2006

## **3 GENERAL**

## 3.1 Description

Blowdown systems are used at petroleum refineries (see SNAP Code 0401) to collect and separate both liquid and vapour discharges from various refinery process units and equipment (U.S. EPA 1985, 1992). The gaseous fraction, that may represent a planned or unplanned hydrocarbon discharge, may be either recycled or flared. Flaring provides a widely-used safety mechanism and emission control option for blowdown systems when the heating value of the emission stream cannot be recovered due to uncertain or intermittent releases during process upsets/emergencies. Non-condensed vapours from the blowdown system may be combusted in a flare which is designed to handle large fluctuations of both the flow rate and hydrocarbon content of the discharge. Alternatively, thermal incineration is preferable to flaring for destroying gas releases that contain more corrosive halogenated or sulphur-bearing components.

Although different types of flares exist, the steam-assisted elevated flare systems are most commonly used at petroleum refineries whereby steam is injected in the combustion zone of the flare to provide turbulence and inspirated air to the flame. For waste gases of insufficient heating value, auxiliary fuels may also be used to sustain combustion.

# 3.2 Definitions

## 3.3 Techniques

Steam-assisted elevated flares are installed at a sufficient height above the plant and located at appropriate distances from other refinery facilities. The flare generally comprises a refractory flame platform with a windshield, steam nozzles, auxiliary gas/air injectors and a pilot burner mounted upon a stack containing a gas barrier. As reported (U.S. EPA 1980, 1992, MacDonald 1990), the flare combustion efficiency typically exceeds 98% with dependence on the following factors (i.e., for efficient performance):

excess steam assist (i.e., steam/fuel gas ratio less than 2),

sufficient gas heating value (i.e., greater than 10 MJ/m3),

low wind speed conditions (i.e., above 10 m/sec.),

sufficient gas exit velocity (i.e., above 10 m/sec.)

Similarly, different types of flare burners, designed primarily for safety requirements, may result in different efficiencies.

# 3.4 Emissions/Controls

Depending on the waste gas composition and other factors, the emissions of pollutants from flaring may consist of unburned fuel components (e.g., methane, NMVOC), by-products of the combustion process (e.g., soot, partially combusted products, CO, CO<sub>2</sub>, NOx) and sulphur oxides (e.g., SO<sub>2</sub>) where sulphur components are present in the waste gas. Steam injection is used to enhance combustion for smokeless burning and to reduce NOx by lowering the flame temperature. Increased combustion efficiency may reduce CH<sub>4</sub> and NMVOC, but will not

reduce  $CO_2$  emissions. Flaring emissions might best be reduced by minimising amounts of gases to be flared, provided that the associated wastes gases are not vented directly.

#### 4 SIMPLER METHODOLOGY

Where limited information is available, the simplest inventory methodology is to combine the amounts of gases flared by petroleum refineries with a single hydrocarbon emission factor (i.e., derived in units of mass emission per volume of gas flared), with the assumption of a constant flare combustion efficiency. In the event that flare gas volumes are unavailable, an alternative but older emission estimation methodology would be to apply individual emission factors of various pollutants for petroleum refinery blowdown systems (i.e., including vapour recovery systems and flaring) in combination with total petroleum refinery feed (i.e., crude oil throughput).

#### **5 DETAILED METHODOLOGY**

The detailed methodology requires each refinery to estimate its flaring emissions using available information on the composition of flare gas, the types of smoke control used and the flare combustion efficiency in combination with flare gas volumes, using either measurement data, available emission factors or mass balance approaches. It is recognised that flare emissions are challenging to estimate and/or quantify with certainty, since: conventional or direct extractive source testing is not feasible for elevated flares; both flare gas volume determinations and/or gas composition may be very uncertain especially during process upsets or emergency releases; and very limited data are available with respect to flare combustion efficiencies which depend on both process and external wind condition factors. For normal operations, the general types of refinery and other information required to estimate flare emissions, as currently done at Canadian refineries (CPPI 1991), are:

- the actual quantities of gases flared at each flare (e.g. m<sup>3</sup>/year) based upon measured flare gas flowmeter or other records,
- the average composition of flare gas including: H/C molar ratio on the basis of flare design or test data, the molecular weight and sulphur content,
- the types of smoke controls used, such as: steam/air, manual/automatic and/or TV monitor,
- an emission HC factor based upon typical steam/fuel gas ratios, gas heating values and/or flare combustion efficiencies,
- a sulphur mass balance of fuels consumed by flaring and other refinery process heaters/boilers.

In some instances, flare emissions may only be estimated currently by difference or rough approximations. However, remote sensing of flare emissions by LIDAR/DIAL measurements of plume cross section seams are assisting in determining or verifying flare emission rates and the composition of refinery flare emissions (Bodon, Moncrieff and Wootton, 1992).

## 6 RELEVANT ACTIVITY STATISTICS

For the simpler methodology, either the quantities of flare gases consumed or the refinery crude oil feed is required. For more detailed methodology, the quantities, composition and heating values of flare gases burned are required for each petroleum refinery.

## 7 POINT SOURCE CRITERIA

All significant refinery flares are to be inventoried as part of refinery point sources.

## 8 EMISSION FACTORS, QUALITY CODES AND REFERENCES

The CONCAWE Air Quality Management Group (Concawe, 2006) has identified a lot of issues with regard to the data submissions for both European Pollutant Emission Register (EPER) mandated by European Directive 96/61/EC on integrated pollution prevention and control (IPPC) and UNECE Kiev Protocol on Pollutant Release and Transfer Registers (PRTR).

In particular CONCAWE initiated a review of the published emission factors for those air pollutants which may be emitted in excess of the EPER threshold values from sources found at the majority of European refineries. CONCAWE, therefore, has drawn up a compendium of emission factors, with associated references, for the uncontrolled release of air pollutants (Concawe, 2006). The compendium can not be considered fully comprehensive as emission factors are not available in the public domain for all sources and/or pollutants. CONCAWE, however, considers this to be the most appropriate set of emissions factors for the refining sector.

The CONCAWE report provides the air pollutant emission estimation algorithms, incorporating those factors, which CONCAWE recommends for EPER and PRTR reporting purposes. The emission factors provided are for uncontrolled releases. Reported emissions must take account of any abatement equipment installed e.g. wet gas scrubbers, electrostatic precipitators, etc. [I assume that for flaring abatement is not relevant] Where emission factors are available, algorithms are provided for sources found in the majority of European refineries.

CONCAWE suggests emission factors for the combustion of the flare gas. For emissions from the combustion of the pilot gas fuel used to initiate flare combustion, they recommend using the combustion emission factors.

The emission factors (Table 2) are available as a function of GJ of flare gas combusted, when mass and composition of the flare stream are known or based on refinery feed (otherwise).

Pollutant	Emission Factor g/GJ of gas flareed (°)	Emission Factor kg/m <sup>3</sup> of refinery feed			
so <sub>2</sub> (°°)	2000000 S	0,077			
NOx	3.22	0.054			
NMVOC	5	0.002			
СО	177	0.012			
PM <sub>10</sub>	Neg	Neg			
$C_6H_6(^{\circ\circ\circ})$	5 B	0.00166			

Table 2:Emission Factors for Refinery Flares

(°) for SO<sub>2</sub>, NMVOC and  $C_6H_6$  expressed as g/ton of gas flared

 $(^{\circ\circ})$  S = mass fraction of sulphur in flare gas

 $(^{\circ\circ\circ})$  B = mass fraction of benzene in flare gas

In U.S. EPA CHIEF database, the VOC emission factor for petroleum refinery flares is: 5.6 lb VOC/million cubic feet of flare gas burned with a quality rating of D. The above mentioned VOC emission factor comprises: methane (20%), ethane (30%), propane (30%) and formaldehyde (20%).

A VOC emission factor, reported in a Norwegian survey (OLF Report Phase 1, Part A), of 0.0095 kg/m3 of flare gas was cited in documentation of the UNECE Task Force - VOC Emissions from Stationary Sources. The flare emissions were reported to consist of 65% methane and 35% NMVOC and suggested a typical flare efficiency of 99.2%.

Remote sensing (DIAL) measurements of full-sized flare emissions at a Norwegian petroleum refinery under normal operating conditions also has indicated that the flare combustion efficiency exceeded 98%, comprising various amounts of methane and C2 to C6+ alkane components (Boden, Moncrieff and Wootton, 1992).

Flare combustion efficiencies, under atypical operating or other conditions and presumably during upset conditions, may have lower destruction efficiencies, based upon other test data (MacDonald 1990).

## 9 SPECIES PROFILES

(See section 8).

## **10 UNCERTAINTY ESTIMATES**

## 11 WEAKEST ASPECTS/PRIORITY AREAS FOR IMPROVEMENT IN CURRENT METHODOLOGY

As flare emissions can vary significantly with dependence on several factors, more measurements to determine flare combustion efficiencies and chemical composition should be done (e.g., perhaps using remote sensing techniques) under a variety of conditions, in order to verify available emission estimates and assure that flare combustion efficiencies generally represent the stated efficiencies.

# 12 SPATIAL DISAGGREGATION CRITERIA FOR AREA SOURCES

# **13 TEMPORAL DISAGGREGATION DATA**

No temporal apportionment of these emissions is possible if the simpler methodology is used. Temporal disaggregation of detailed emission estimates can be done from records of petroleum refinery shutdowns and other operating data.

# 14 ADDITIONAL COMMENTS

## **15 SUPPLEMENTARY DOCUMENTS**

## **16 VERIFICATION PROCEDURES**

As noted above, remote sensing monitoring programs may be useful to verify flaring emission estimates.

## **17 REFERENCES**

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## **18 BIBLIOGRAPHY**

## **19 RELEASE VERSION, DATE AND SOURCE**

Version: 1.4

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Source: Marc Deslauriers Environment Canada Canada Revised and integrated with CONCAWE (CONCAWE, 2006) data by: Carlo Trozzi Techne Consulting Italy

#### **20. POINT OF ENQUIRY**

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